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2 **Title** - Shoes alter the spring-like function of the human foot during running

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28 **Keywords** – Barefoot running, intrinsic foot muscles, longitudinal arch, leg-spring mechanics

29

1 **Abstract**

2 The capacity to store and return energy in legs and feet that behave like springs is crucial to
3 human running economy. Recent comparisons of shod and barefoot running have led to
4 suggestions that modern running shoes may actually impede leg and foot spring function by
5 reducing the contributions from the leg and foot musculature. Here we examined the effect of
6 running shoes on foot longitudinal arch motion and activation of the intrinsic foot muscles.
7 Participants ran on a force-instrumented treadmill with and without running shoes. We recorded
8 foot kinematics and muscle activation of the intrinsic foot muscles using intramuscular
9 electromyography. In contrast to previous assertions, we observed an increase in both the peak
10 (flexor digitorum brevis +60%) and total stance muscle activation (flexor digitorum brevis
11 +70%, abductor hallucis +53%) of the intrinsic foot muscles when running with shoes.
12 Increased intrinsic muscle activation corresponded with a reduction in longitudinal arch
13 compression (-25%). We confirm that running shoes do indeed influence the mechanical
14 function of the foot. However, our findings suggest that these mechanical adjustments are likely
15 to have occurred as a result of increased neuromuscular output, rather than impaired control as
16 previously speculated. We propose a theoretical model for foot-shoe interaction to explain these
17 novel findings.

18

19 **Introduction**

20 It has been suggested that humans may have evolved to run and have done so for millions of
21 years [1,2]. Hard surfaces have been encountered by humans when running throughout
22 evolution, however the modern running environment, characterised by stiff, invariant substrates
23 such as roads and footpaths, has transformed at a far greater rate than evolution can progress
24 [1-3]. The apparent lack of natural variability in surface terrain and compliance that is endemic
25 in our modern running world is believed to have altered the biomechanical demands of running
26 [4,5], possibly contributing to the high injury rate in those who habitually partake in this activity
27 [6].

28

29 The human foot is the interface between the body and the ground. The unique structure of the
30 foot allows force produced by muscles of the lower limb to be transmitted to the ground, to
31 support body weight and also generate forward propulsion [7,8]. A pronounced structural
32 feature of the human foot is the longitudinal arch (LA), which allows the foot to function in a
33 spring-like manner [1,2,9,10] in series with the entire lower limb [11,12]. The LA compresses

1 during early stance, absorbing mechanical energy as the ground reaction force increases.
2 Presumably the energy absorbed is stored within elastic structures supporting the arch
3 [9,13,14]. In late stance, when ground reaction force decreases, the LA recoils, returning elastic
4 energy to deliver power for propulsion [9]. Stiffness of the LA is provided by passive
5 ligamentous structures [9,14,15] acting in parallel with the intrinsic foot muscles whose relative
6 contribution is continually adjusted by the central nervous system (CNS) in response to
7 mechano-sensory stimuli [10,16]. This elegant arrangement allows the mechanical
8 characteristics of the foot to be rapidly adapted to loading or task demands [10] and is thought
9 to improve the efficiency of human running, returning between 8 and 17% of the mechanical
10 energy required for one stride, via passive mechanisms alone [9,13].

11
12 Footwear has provided mechanical and thermal protection for human feet when running, for
13 thousands of years [17]. The contemporary running shoe, however, was not invented until the
14 1970's [18] and has evolved in parallel with the surge in popularity of running as a recreational
15 pursuit. A defining characteristic of the modern running shoe is the thick visco-elastic midsole
16 that is designed to compress and rebound when cyclically loaded and unloaded during running
17 [19,20]. This design feature, generally referred to as cushioning, allows the shoe to function in
18 a similar "spring-like" manner to the lower limb and foot, absorbing the potentially harmful
19 impact transients that are encountered when the foot impacts with the ground [21-24], while
20 also returning some of this energy to aid power generation for propulsion [25]. Another key
21 feature of the modern running shoe is the contoured midsole, designed to provide external
22 support and reduce excessive strain on the muscles and ligaments of the LA [21].

23
24 However, despite the huge financial investment in the development of running shoes, running
25 injury rates remain relatively unchanged over the last 40 years [6,26,27], leading some to
26 question the efficacy of modern running shoes in preventing injury [3,28-31]. Some scholars
27 have gone as far to suggest that cushioned midsoles may actually hinder our running
28 performance [3,28-30,32]. These scholars have speculated that a thick cushioned interface
29 between the runner and the ground impairs mechano-sensory feedback and therefore, the
30 inherent capacity of the CNS to contend with large impact force transients via adjustments in
31 leg- and foot-spring stiffness [3,29,33]. Furthermore, it has been speculated that an apparent
32 reliance on the shoe to attenuate impact and provide mechanical support for the LA may reduce
33 the required contributions from the foot and ankle musculature, precipitating foot and ankle
34 muscle weakness and predisposing a runner to injury [28,31,34]. While there is some evidence

1 that runners tend to land differently when they run without shoes [28,35-38], there is no
2 evidence that shoes have a detrimental influence on the spring-like function of the foot, or the
3 contributions to this function from foot and ankle musculature.

4
5 Despite the on-going speculation as to the potential benefits and detrimental effects that modern
6 running shoes may have on running mechanics, it is apparent that there is a dearth of
7 information pertaining to how the CNS regulates the spring-like function of the foot during
8 shod running. Therefore, the aim of this study was to test the hypothesis that running shoes
9 impair the spring-like function of the foot, thereby altering the required force contribution from
10 the intrinsic foot muscles to actively support the LA during running. In order to test this
11 hypothesis, we had participants run on a force-instrumented treadmill barefoot and wearing
12 running shoes. In addition to the ground reaction forces (GRF), electromyograms (EMG) were
13 recorded from the intrinsic foot muscles and ankle plantar flexors, while motion capture data
14 were recorded to assess foot and ankle kinematics during multiple consecutive strides.

16 **Methods**

17 **Participants**

18 Sixteen healthy participants (seven females mean \pm standard deviation for age 19 ± 1 years;
19 height: 165 ± 4 cm; mass: 59 ± 7 kg, nine males age 24 ± 5 years; height: 172 ± 4 cm; mass: 73
20 ± 10 kg) with no history of lower limb injury in the previous six months or known neurological
21 impairment volunteered to participate in the study. All participants were habitually shod
22 recreational runners. Foot-strike technique (ie. rear-foot or forefoot) was not applied as an
23 inclusion or exclusion criteria, however none of the participants recruited for this study
24 displayed a forefoot running technique when either shod or barefoot. Written informed consent
25 was obtained from each subject. The study protocol was approved by the institutional human
26 research ethics committee and conducted in accordance with the Declaration of Helsinki.

28 **Experimental Protocol**

29 Following a 3-min warm up period and familiarisation procedure, participants ran on a force-
30 instrumented treadmill (AMTI, force-sensing tandem treadmill, Watertown, MA, USA) at 14
31 $\text{km}\cdot\text{h}^{-1}$ while barefoot and shod. The running shoe chosen for this study is described by the
32 manufacturer as a “cushioned stability” shoe, with a heel height of 30mm and forefoot height
33 of 20mm (Asics GT2000, Asics Corp. Japan). The inner lining was made of soft, flexible foam.

1 In order to prevent rubbing against the intramuscular electrodes, the raised edges of the inner
2 lining were trimmed flat and had no contact with the skin of the LA. Kinetic, kinematic and
3 EMG data were collected simultaneously with approximately 15-20 strides (toe-off to
4 ipsilateral toe-off) being recorded for each condition (barefoot and shod).

5

6 Data Acquisition

7 *Kinematic and kinetic measurements*

8 Three-dimensional (3D) motion of the foot and shank, and GRF data were collected during
9 each running trial. Retro-reflective markers (9.0 mm diameter) were secured on the skin of the
10 right foot, overlying the medial and lateral malleoli, posterior calcaneus, navicular tuberosity
11 and head of the first and fifth metatarsals, in order to quantify motions of the foot segments and
12 the LA (Figure 1). Additional markers were applied to the medial and lateral femoral condyles
13 and a rigid cluster of four markers was placed on the antero-lateral aspect of the shank. During
14 a standing calibration trial, markers located on the segment endpoints were used to generate a
15 two-segment model of the shank and foot. Following the calibration trial, the medial and lateral
16 knee markers were removed and the motion of the shank was tracked with the
17 rigid marker cluster. In order to allow foot marker positions to be captured during the shod
18 condition, circular holes of 25 mm diameter were cut in the shoe upper in positions
19 corresponding to the foot marker locations. This allowed visualisation of the markers, while
20 still allowing markers to be adhered to the skin. Markers were adhered with double sided
21 adhesive and further secured with cohesive bandage, allowing secure positioning for both the
22 shod and barefoot conditions.

23

24 Kinematic data were captured at 200 Hz using an eight camera 3D optoelectronic motion
25 capture system (Qualysis, Gothenburg, Sweden) while GRF and EMG data were synchronously
26 captured at 4000 Hz via a 14-bit analogue to digital converter (Qualysis, Gothenburg, Sweden).
27 Kinematic, force and EMG data were collected simultaneously and synchronized using the
28 Qualysis Track Management software from the same company.

29

30 *Electromyography*

31 Identification of the abductor hallucis (AH) and flexor digitorum brevis (FDB) muscles was
32 conducted using real-time B-mode ultrasound imaging (10 MHz linear array, Ultrasonix RP,
33 USA) in the right foot of each subject. Subsequently, bi-polar fine-wire electrodes (0.051 mm
34 stainless steel, Teflon coated, Chalgren, USA) with a detection length of 2 mm and inter-

1 electrode distance of 2 mm were inserted using delivery needles (0.5 mm x 50 mm) into the
2 muscle tissue of AH and FDB under ultrasound guidance, in accordance with previously
3 described methods [39]. Sterile techniques were used for the insertion of all wires. Surface
4 EMG data were collected from medial gastrocnemius (MG) and soleus (SOL) from the right
5 leg of all participants using Ag-AgCl electrodes with a diameter of 10 mm and an inter-
6 electrode distance of 20 mm (Tyco Healthcare Group, Neustadt, Germany). A surface reference
7 electrode (10 mm diameter, Ag/AgCl, Tyco Healthcare Group, Neustadt, Germany) was placed
8 over the right fibula head. Prior to electrode placement, the areas of the leg corresponding to
9 the electrode placement sites were shaved, lightly abraded and cleaned with isopropyl alcohol.

10

11 All EMG signals were amplified 1000 times and recorded with a bandwidth of 30 -1000 Hz
12 (MA300, Motion Labs, LA, USA). In order to minimise movement artefacts, the fine-wire
13 electrodes, surface electrodes, connectors, cabling and pre-amplifiers were secured with
14 cohesive bandage around the foot and shank.

15

16 Prior to data collection, each participant was asked to perform foot manoeuvres known to
17 activate each foot muscle separately [16,40]. When predicted EMG patterns could be detected,
18 it was concluded that the fine-wire electrodes were in the correct location. If not, the electrodes
19 were withdrawn by approximately 1mm until appropriate activation patterns could be detected
20 and possible crosstalk excluded. In order to ensure quality of the intramuscular EMG signal
21 throughout the experiment, signal quality was assessed following each experimental condition
22 using the same technique described above. A Velcro strap was secured around the participant's
23 waist, which enabled the EMG amplifier box to be secured to the subject without interfering
24 with their gait. A lightweight optical cable connected the amplifier box to the analogue to digital
25 converter.

26

27 Data analysis

28 Kinetic and kinematic data files were exported to Visual3D (C-motion Inc., Germantown, MD,
29 USA) for analysis. Force plate data recorded during each experimental trial was digitally
30 filtered with a recursive 35 Hz low pass, fourth order Butterworth filter. A vertical GRF
31 threshold was set to define each toe-off as occurring when vertical GRF fell below 50 N, while
32 foot contact was defined as occurring when vertical force rose above 50 N. Swing phase was
33 defined as the period from right toe-off to right foot contact, while stance phase was defined as

1 occurring between right foot contact and right toe-off. One stride cycle was defined as occurring
2 from right toe-off to the subsequent right foot toe-off.

3
4 Subsequently the magnitude of the vertical and antero-posterior (A-P) components of the GRF
5 were calculated and normalised to bodyweight for each participant. Peak loading rate was
6 defined as the maximum value obtained from the first derivative of the vertical GRF in the first
7 50ms following foot contact, while peak propulsive force was defined as the peak positive value
8 of the A-P component of the GRF.

9
10 Marker trajectories were digitally filtered with a recursive 20 Hz low pass, fourth order
11 Butterworth filter. Assumed rigid segments were created for the shank and foot. Joint rotations
12 were calculated in accordance with International Society of Biomechanics recommendations
13 (+y up, +z medial, +x anterior) with rotation about the z-axis - sagittal plane motion, rotation
14 about the x-axis – frontal plane motion and rotation about the y-axis – transverse plane motion
15 [41]. Ankle angle was defined as the angle of the foot segment relative to the shank, with plantar
16 flexion reported as a positive angular rotation. Ankle angle at contact was calculated as the
17 sagittal plane ankle angle at foot contact and ankle excursion was calculated by subtracting the
18 minimum ankle angle during stance phase from the ankle contact angle. The LA angle was
19 defined as a sagittal planar angle created by the bisection of a vector projecting from the medial
20 malleolus marker to the navicular marker and another vector projecting from the head of the
21 first metatarsal to the navicular marker (Figure 2). Thus a decrease in LA angle is indicative of
22 a reduction in LA height. In order to describe the spring-like behaviour of the LA during stance
23 phase, measures of compression and recoil were calculated. Compression of the LA was defined
24 as the reduction in LA angle (height) that occurs due to the application of load reduction and
25 was calculated by subtracting the minimum LA angle during stance phase from the LA angle
26 at foot contact. LA recoil was defined as the increase in LA angle (height) that occurs during
27 unloading and was calculated by subtracting the minimal LA angle during stance phase from
28 the LA angle at toe-off.

29
30 Due to technical difficulties associated with collecting intramuscular EMG data from the foot
31 muscles within a running shoe, complete sets of muscle activation data from AH and FDB was
32 only obtainable from 10 of the 16 participants, while surface EMG data from MG and SOL was
33 collected from all participants. The EMG data were exported to Spike2 software (Cambridge
34 Electronic Design, Cambridge, UK) prior to analysis. All signals were high-pass filtered using

1 a recursive fourth order Butterworth filter at 35 Hz to remove any unwanted low-frequency
2 movement artefact. The EMG signals were then visually inspected in order to identify any
3 remaining artefact, which was defined as an abnormal spike in the signal, typically associated
4 with foot contact. Any such remaining artefacts resulted in the EMG data for that particular
5 stride being excluded from further analysis. Following DC-offset removal, root mean square
6 (RMS) signal amplitude was calculated using a moving window of 50 ms to generate an EMG
7 envelope. Subsequently, the EMG envelope for each muscle was normalised to its peak
8 amplitude found across all conditions. Normalised peak EMG amplitude and total stance
9 activity (based on the EMG envelope) was calculated during the stance phase for each stride
10 cycle, allowing comparisons in magnitude of stance phase muscle activation between shod and
11 unshod conditions. In order to provide insight into the magnitude of activation relative to the
12 time that a muscle is generating force, total stance phase activity (%max.s) was calculated by
13 multiplying the mean normalised RMS signal amplitude during stance (%max) by the mean
14 stance phase duration (s) for each muscle and condition [42,43].

15

16 For each individual, the kinematic, kinetic and EMG data were averaged across a minimum of
17 10 stride cycles to form individual variable means for each condition.

18

19 *Statistics*

20 Paired t-tests were used to describe the influence of running shoes on stride temporal
21 characteristics, peak vertical ground reaction force, peak loading rate, peak propulsive force,
22 ankle contact angle, ankle excursion, LA compression and recoil and peak muscle activation.
23 Statistical differences were established at $P \leq 0.05$. Results are presented as mean \pm standard
24 deviation (SD) unless otherwise stated.

25

26 **Results**

27 *Running mechanics*

28 Shod running was typified by a longer stride duration (shod 0.68 ± 0.03 s vs. barefoot $0.65 \pm$
29 0.03 s, $P \leq 0.05$) and ground contact times (shod 0.21 ± 0.01 s vs. barefoot 0.18 ± 0.01 s, $P \leq$
30 0.05). When running shod and barefoot, participants produced comparable magnitudes of
31 vertical ground reaction forces (shod 2.75 ± 0.24 body weights (BW) vs. barefoot 2.75 ± 0.22
32 BW, $P = 0.6$), however mean peak loading rate (shod 74.5 ± 10.0 BW s^{-1} vs. barefoot $86.4 \pm$
33 14.2 BW s^{-1}) and mean peak propulsive force (shod 0.41 ± 0.05 BW vs. barefoot 0.44 ± 0.05
34 BW) were both reduced when running with shoes (both $P \leq 0.05$, Figure 3). Participants

1 adjusted the angular orientation of the ankle at foot contact depending on the running condition
2 ($P \leq 0.05$), adopting a position of slight dorsiflexion when running in shoes ($2.0 \pm 2.8^\circ$, range
3 $-7.1 - 1.9^\circ$, Figure 4), while they landed in a position of slight plantar flexion when running
4 barefoot ($1.8 \pm 2.3^\circ$, range $-5.3 - 4.7^\circ$).

5
6 For shod and barefoot conditions, ankle dorsiflexion occurred following forefoot contact in
7 early stance, until late stance when the ankle underwent rapid plantar flexion. Ankle
8 dorsiflexion excursion was significantly less when running with shoes (shod $14.8 \pm 4.6^\circ$ vs.
9 barefoot $20.3 \pm 6.8^\circ$, $P \leq 0.05$), due to a more plantar flexed position of the ankle at initial foot
10 contact and similar peak dorsiflexion angles during mid- to late-stance (Figure 4).

11
12 The LA compressed, during early to mid-stance as the vertical ground reaction force was rising
13 and recoiled during late stance as the vertical ground reaction force subsided (Figure 4). The
14 LA angle at foot contact was similar for both conditions (shod $150.4 \pm 9.9^\circ$ vs. barefoot 151.0
15 $\pm 9.6^\circ$, $P = 0.4$). However, when running with shoes, participants displayed reduced magnitudes
16 of both LA compression (shod $8.6 \pm 4.6^\circ$ vs. barefoot $11.5 \pm 4.0^\circ$ $P \leq 0.05$) and recoil (shod
17 $15.4 \pm 5.7^\circ$ vs. barefoot $21.5 \pm 5.5^\circ$, $P \leq 0.05$) primarily due to a combination of a lower
18 minimum LA angle at mid-stance and a higher LA angle at propulsion (Figure 4). When
19 considered together, the reduction in LA compression and similar peak ground reaction forces,
20 intimate that the LA is stiffer in the shod condition.

21 22 *Muscle activation*

23 The FDB and AH muscles recorded intramuscularly, displayed similar patterns of activation
24 within each condition. Both showed periods of relative inactivity during swing and large bursts
25 of activity during stance (Figure 4). Peak activation generally occurred during mid-stance for
26 both muscles. Total stance activity was higher when running with shoes, for both FDB (shod
27 $7.1 \pm 2.7\%$ max.s vs. barefoot $4.2 \pm 3.4\%$ max.s, $P \leq 0.05$) and AH (shod $6.3 \pm 2.0\%$ max.s vs.
28 barefoot $4.1 \pm 1.8\%$ max.s, $P \leq 0.05$). Peak FDB activation was greater when running with
29 shoes, compared to barefoot (shod $64.8 \pm 25.9\%$ vs. barefoot $40.7 \pm 19.0\%$, $P \leq 0.05$, Figure
30 4), while no consistent differences were observed between the shod and unshod conditions for
31 AH (shod $56.2 \pm 19.3\%$ vs. barefoot $45.4 \pm 19.3\%$, $P = 0.17$, Figure 4).

32
33 Soleus and MG muscles were both relatively quiescent during early swing phase, with a large
34 burst of activity that commenced during terminal swing and peaked prior to mid-stance (Figure

1 4). Total stance activity was higher when running with shoes, for both MG (shod 7.1 ± 2.4
2 %max.s vs. barefoot 5.9 ± 3.3 %max.s, $P \leq 0.05$) and SOL (shod 6.1 ± 1.2 %max.s vs. barefoot
3 5.0 ± 0.7 %max.s, $P \leq 0.05$). Peak MG activity was greater when running with shoes (shod 65.6
4 ± 15.4 % vs. barefoot 57.6 ± 16.2 %, $P \leq 0.05$, Figure 4) while no significant differences were
5 observed in SOL activity between the shod and unshod conditions (shod 64.8 ± 15.4 % vs.
6 barefoot 59.0 ± 14.6 %, $P = 0.09$).

7 8 **Discussion**

9 This study provides novel evidence of adjustments in the mechanical function of the foot when
10 comparing running in shoes to barefoot. In line with our first hypothesis, running with shoes
11 led to a reduction in the magnitude of LA compression and recoil, suggesting that running shoes
12 influence foot-spring function. Of particular interest was the underlying mechanism for the
13 observed alterations in LA motion when running in shoes, which we believe is at least
14 partially driven by an increase in neuromuscular output, rather than a decrease, as we
15 originally hypothesised.

16 17 *Stance phase*

18 During stance, the lower limbs of human runners behave in a spring-like manner, “compressing
19 and recoiling” via concurrent ankle, knee and hip joint flexion then extension, in phase with the
20 increasing and decreasing magnitude of the vertical ground reaction force
21 [12,44,45]. This highly efficient mechanism allows recycling of elastic and kinetic energy
22 during each foot contact [11,46], while also allowing a relatively stable centre of mass trajectory
23 [45]. The central nervous system has the capacity to adjust the stiffness of the lower limb in
24 order to minimise centre of mass vertical motion when running across terrains with varying
25 undulations [47] and compliance [45,48,49]. The foot is considered a key contributor to leg-
26 spring function [9,10,12,13] however to date, we believe, the influence of running shoes on the
27 spring-like function of the foot has not been reported.

28
29 Runners in our experiment displayed substantially less arch compression and recoil when
30 running with shoes, as compared to barefoot. This finding is in line with the key design features
31 of running shoes that aim to provide support for the LA and reduce strain on plantar soft-tissue
32 structures [50,51]. However, this finding also highlights that running shoes may actually limit
33 the capacity for the foot to store and return energy via elastic mechanisms, due to a reduction
34 in the magnitude of arch compression and recoil [13]. A key argument of those who repudiate

1 the efficacy of modern running footwear is the potential for the cushioning and support
2 characteristics of the shoe to impair foot-spring function, with a likely consequence of reduced
3 activation from muscles that support the arch, leading to their weakness and disuse atrophy
4 [3,29,34]. Our findings partially support this notion. However, the observed concomitant
5 increase in intrinsic foot muscle activation in shod running appears to indicate that the reduced
6 arch compression observed when running with shoes is driven by an increase in muscle
7 activation, rather than via the cushioning and external support features of the running shoes.

8
9 In a recent series of experiments we provided novel evidence that the intrinsic foot muscles
10 function in parallel with the plantar aponeurosis, actively tuning the stiffness of the LA in
11 response to load during stance and locomotion [10,16,39]. Employing intramuscular electrical
12 stimulation to activate individual intrinsic foot muscles, it was observed that contraction of
13 these muscles could produce a 5% increase in arch height, reversing the compression of the LA
14 that occurred when the foot was loaded with forces equivalent to bodyweight [16]. Given that
15 the intrinsic foot muscles are known to act in unison as a functional group [10,52], it is likely
16 that their combined action and the action of the extrinsic muscles [53,54] may have a profound
17 effect on LA function. Therefore when considering the findings of the current study with those
18 of our earlier studies, it becomes apparent that the observed increase in intrinsic foot muscle
19 activation when running with shoes, compared to barefoot, is likely to be partially responsible
20 for the concomitant reduction in LA compression during stance.

21
22 Given that the LA acts as a spring with an actively adjustable stiffness [9] and running shoes
23 with visco-elastic midsoles also behave in a spring-like manner [23,25], the foot and shoe can
24 be modelled to behave as two springs acting either in parallel, or in series, during the stance
25 phase (Figure 4). Modelling the interaction between running shoes and the LA, potentially
26 allows us to reveal the underlying mechanism for the observed increase in muscle activity when
27 running in shoes. Within this model, the LA behaves as a single spring of given stiffness (k_{foot})
28 that is continually adjusted via activation of the muscles that span the arch of the foot [16], in
29 order to optimise forces acting between the body and the ground. For example, intrinsic foot
30 muscle activation increases when running at faster velocities, stiffening the LA and thereby
31 allowing greater forces to be transmitted between the body and ground during shorter ground
32 contact periods [10]. When a runner wears shoes with a visco-elastic midsole, the shoe will
33 behave as an additional spring, also with a given stiffness (k_{shoe} , Figure 5) and the two form a

1 foot-shoe system that has a stiffness (k_{FS}) that is dependent on the configuration of the two
2 springs.

3

4 If the arch and shoe springs are modelled to be in parallel, the net stiffness of the foot-shoe
5 system (k_{FS}) is the summed stiffness of the longitudinal arch (k_{foot}) and shoe (k_{shoe}) springs
6 acting together.

7

$$k_{FS} = k_{foot} + k_{shoe}$$

8

9 Alternatively, if we model the foot and shoe as springs acting in series, the net compliance
10 (inverse of stiffness) of the foot-shoe system ($1/k_{FS}$) will be the common compliance of the
11 longitudinal arch ($1/k_{foot}$) and shoe ($1/k_{shoe}$) springs acting together.

12

$$1/k_{FS} = 1/k_{foot} + 1/k_{shoe}$$

13

14 To interpret both of these models with our data, we will assume that the neuromuscular system
15 seeks to maintain a constant overall lower limb stiffness, including a constant K_{FS} . This
16 assumption is based on a wealth of prior studies showing that humans adjust muscle activations
17 to maintain constant system stiffness on surfaces of varied compliance [45,48,55,56] and also
18 when wearable devices are added to the limb that influence system stiffness [57-59].

19

20 For our model of springs in parallel ($k_{FS} = k_{foot} + k_{shoe}$) if a runner wears running shoes of a
21 given stiffness, the addition of the shoe spring will lead to an overall increase in k_{FS} . Thus,
22 under the assumption that constant system stiffness is beneficial during constant velocity
23 running [45,48,60], a reduction in LA stiffness is required in order to offset the additional
24 stiffness added by the shoe. Reduced longitudinal arch stiffness would be achieved by
25 allowing greater arch compression, presumably through a reduction in force output from the
26 arch musculature; neither of which were observed here.

27

28 If the model of springs in series is considered ($1/k_{FS} = 1/k_{foot} + 1/k_{shoe}$) running in shoes with a
29 visco-elastic midsole will decrease k_{FS} due to the presence of an additional spring. Therefore,
30 an increase in longitudinal arch stiffness is necessary to increase overall system stiffness,
31 maintaining constant k_{FS} . An increase in longitudinal arch stiffness would require a reduction
32 in longitudinal arch compression, which is achievable via an increase in force output from the
33 intrinsic foot muscles (increased activation) [10]. This is in line with our observations that

1 intrinsic foot muscle activation increased and longitudinal arch compression decreased, when
2 running in shoes.

3

4 According to the above scenarios that describe the potential interactions between human feet
5 and running shoes, it seems that running shoes act as an additional spring in-series with the
6 foot. While we cannot discount that deformation of the shoes may act to provide supporting
7 forces to LA, an in-series spring model provided a sound mechanical rationale for our finding
8 that running in shoes induced an increase in muscle activation from two of the primary muscles
9 within the LA. The incorporation of intrinsic foot muscle activation data has therefore provided
10 a unique insight into the underlying mechanism for the observed changes in LA function when
11 running in shoes. Most importantly, these findings highlight that the alterations in lower limb
12 biomechanics observed when running in shoes are not a result of reduced or impaired
13 neuromuscular function.

14

15 The increase in ankle plantar flexor activation and reduction in ankle dorsiflexion observed
16 when our runners were shod indicates that our runners may have also exhibited an increase in
17 ankle stiffness in response to the increased compliance provided by the running shoe. Increased
18 knee and ankle stiffness has previously been observed when running in shoes with visco-elastic
19 midsoles [20,23] indicating that the cushioning properties of shoes may induce similar
20 mechanical adaptations across the entire lower limb. This finding provides further support for
21 our model that describes running shoes as springs acting in-series with the foot and leg.
22 Furthermore, these findings are in line with previous research describing the in-series
23 interaction between the lower limb and running support surface [48] and the apparent increase
24 in leg stiffness that is observed when running on compliant surfaces [45,61].

25

26 *Impact phase*

27 The initial impact phase can be described to occur over the first 50 ms of ground contact and
28 involves the rapid deceleration of the lower limb that occurs when the foot and ground collide
29 [62] with forces up to twice bodyweight being transmitted at rates of up to 200 bodyweights
30 per second [28,63]. Impact loading rates are considerably higher on stiff surfaces such as
31 concrete, which are endemic in our modern running environment [64] and possibly contribute
32 to the high prevalence of repetitive stress injury in runners [65]. The modern running shoe been
33 designed to reduce the rate of force increase during the impact phase, thereby reducing the risk
34 of injury to the runner. However, a counter argument has been raised that suggests that the

1 presence of a cushioned midsole lends to the adoption of a marked heel-first landing pattern
2 and a reliance on the shoe to attenuate impact, rather than via the body's natural shock
3 absorbers: muscle and tendon [28,29]. Within the current experiments, our runners adopted a
4 heel-strike pattern when running in shoes, while they contacted the ground with their mid-foot
5 when barefoot. This finding is consistent with a number of previous comparisons of shod and
6 un-shod running in runners who habitually wear shoes, further confirming that runners
7 generally impact the ground differently when running in shoes as compared to barefoot
8 [4,5,28,63,66]. It has been reported that barefoot runners tend to strike the ground with a
9 forefoot first contact, allowing the body to effectively damp the large impact transients [67-69]
10 via controlled dorsiflexion of the ankle and the associated stretch of the Achilles tendon [68].
11 Interestingly, despite our runners adopting a more plantar flexed ankle position when running
12 without shoes, peak-loading rates still remained considerably higher. Thus, despite the
13 modification in landing mechanics, the magnitude of adaptation in our habitually shod runners
14 was insufficient to damp impacts in a manner comparable to the cushioned running shoe.
15 Further research may elucidate if these observations persist across habitually barefoot running
16 populations.

17

18 *Methodological considerations*

19 There are some methodological considerations that should be taken into account when
20 considering these data. Within the present study we have attributed the observed increase in LA
21 stiffness when running with shoes to an increase in intrinsic foot muscle activation. It is likely
22 that other muscles such as tibialis posterior and the long digital flexors may have also
23 contributed to the observed alteration in LA mechanics, as these muscles are also known to
24 provide active support for this structure [53,54,70,71].

25

26 Our measure of "total stance activation" was calculated by multiplying the average of the RMS
27 signal envelope during stance, by the stance phase duration for each condition. This calculation
28 was adopted to provide an indication of the cost of muscle activation per step, taking into
29 account the differences in stance phase duration between conditions [42,43]. Participants ran
30 with a reduced cadence (longer stride duration) when shod, and thus, it may be suggested that
31 the observed increase in total stance phase activation when shod may be offset by fewer strides
32 in a minute. However within the current study this is not the case, as the difference in cadence
33 between the two conditions is considerably smaller in magnitude than the difference in total
34 stance activation. Based on the data presented in the manuscript, the average strides per minute

1 for the barefoot condition is 92.3, while for the shod condition it is 88.2. If the total strides in a
2 minute are multiplied by the total stance activity for the muscle with the smallest difference
3 (AH), the shod condition has approximately 46% more activation per minute than the barefoot
4 condition (shod 555.1 total stance activity·min⁻¹ v barefoot 378.4 total stance activity·min⁻¹).

5
6
7 In our discussion of the foot and shoe interaction, we have made the assumption that constant
8 leg stiffness is ideal during steady state running. This assumption is based on a growing body
9 of evidence that indicates the CNS will adjust knee and ankle stiffness in order to maintain
10 constant COM trajectory [45,48,55,56]. Further research is now required to determine if the
11 foot behaves in series with the ankle and knee to govern overall limb stiffness during running,
12 while also examining if the observed changes in LA stiffness during running are primarily due
13 to an alteration in surface compliance.

14 15 *Conclusion*

16 In summary, we have described a novel mechanism for how human feet interact with modern
17 running shoes. An in-series, spring-like arrangement of the foot and shoe dictates that the
18 reduction in system stiffness that occurs when wearing a running shoe will need to be offset by
19 an increase in the stiffness of the longitudinal arch, in order to maintain constant foot-shoe
20 system stiffness. The observed increase in longitudinal arch stiffness in response to mechano-
21 sensory stimuli, is likely achieved via the observed increase in activation from the intrinsic
22 muscles of the arch. These findings further highlight the highly adaptable nature of the human
23 foot and it's importance in upright bipedal locomotion.

24 25 **Author Contributions**

26 LK – study design, data collection and analysis, manuscript preparation

27 GL - study design, data analysis and manuscript preparation

28 DF - data analysis and manuscript preparation

29 GL - study design, data analysis and manuscript preparation

30 31 **Competing interests**

32 Funding for this study was provided by Asics Oceania Pty. Ltd.

33 34 **Acknowledgments**

1 The authors would like to acknowledge Mr Zachary Goodchild for his contributions to data
2 collection and processing.

3

4 **Funding**

5 Funding for this study was provided by Asics Oceania Pty Ltd. Grant ID number 2014000885.

6

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20

21 **Figure Legends**

22 **Figure 1.** Depiction of the Lower limb marker set employed for collection of kinematic data.
23 White markers are removed following a static calibration trial, with the cluster of four markers
24 on a rigid plastic shell used to track the motion of the shank.

25

26 **Figure 2.** Longitudinal arch angle is defined as the angle created by the bisection of a vector
27 projecting from a marker located on the medial malleolus (A) to a marker located on the
28 navicular tuberosity (B), with a vector projecting from a marker located on the head of the first
29 metatarsal (C) to a marker on the navicular tuberosity (B). A reduction in longitudinal arch
30 angle indicates arch compression, while an increase in arch angle indicates arch recoil.

31

32 **Figure 3.** Group mean \pm standard deviation (shaded area) for vertical force (top), vertical force
33 loading rate (middle) and antero-posterior force (bottom). Data is recorded from each
34 participant running barefoot (red) and shod (blue) at 3.89 ms⁻¹ and presented from from foot

1 contact to toe off from the right foot. Loading rate is defined as the first derivative of the vertical
2 ground reaction force signal. All data is normalised to body weight.

3

4 **Figure 4.** Group mean ensembles \pm standard deviation (shaded area) for changes (Δ) in
5 longitudinal arch (LA) and ankle angle (degrees, $^{\circ}$, top), electromyography (EMG) normalised
6 root mean square signal amplitude for flexor digitorum brevis (FDB) and abductor hallucis
7 (AH), gastrocnemius medialis (MG) and soleus (Sol). Group mean ensembles are defined from
8 toe off (TO) to ipsilateral toe off for the right foot. Data recorded during running at 3.89 ms^{-1} .
9 For each muscle EMG data is normalised to the maximal amplitude recorded for all trials.
10 Change in LA and ankle angle was calculated by subtracting the angle at foot contact in the
11 barefoot condition from the angle-time data from both shod and barefoot conditions. FC, foot
12 contact. The barefoot condition is the red dashed lines and shod the solid blue lines

13

14 **Figure 5.** Depiction of a parallel (top) and in-series (bottom) spring arrangement between the
15 longitudinal arch and running shoe. Both the longitudinal arch and running shoe will behave in
16 a spring-like manner during running, compressing and recoiling as force is increased and
17 decreased. If the longitudinal arch and running shoe act in-parallel, wearing a running shoe will
18 increase the overall stiffness of the foot-shoe system. If the longitudinal arch and running shoe
19 act in-series, wearing a running shoe will increase the overall compliance of the foot-shoe
20 system. Based on the assumption that constant foot-shoe system stiffness is favoured during
21 steady state running, the response of the intrinsic foot muscles in regulating the stiffness of the
22 arch will vary depending on whether the longitudinal arch and running shoe behave in-parallel
23 or in-series.

24

25

26

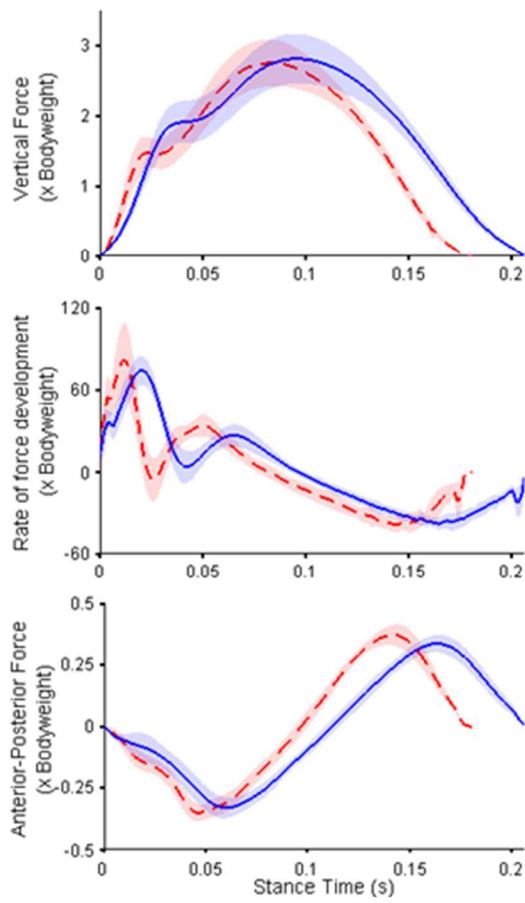


Figure 1. Group mean \pm standard deviation for vertical force (top), vertical force loading rate (middle) and antero-posterior force (bottom). Data is recorded from each participant running barefoot (red) and shod (blue) at 3.89 ms^{-1} and presented from from foot contact to toe off from the right foot. Loading rate is defined as the first derivative of the vertical ground reaction force signal. All data is normalised to body weight.

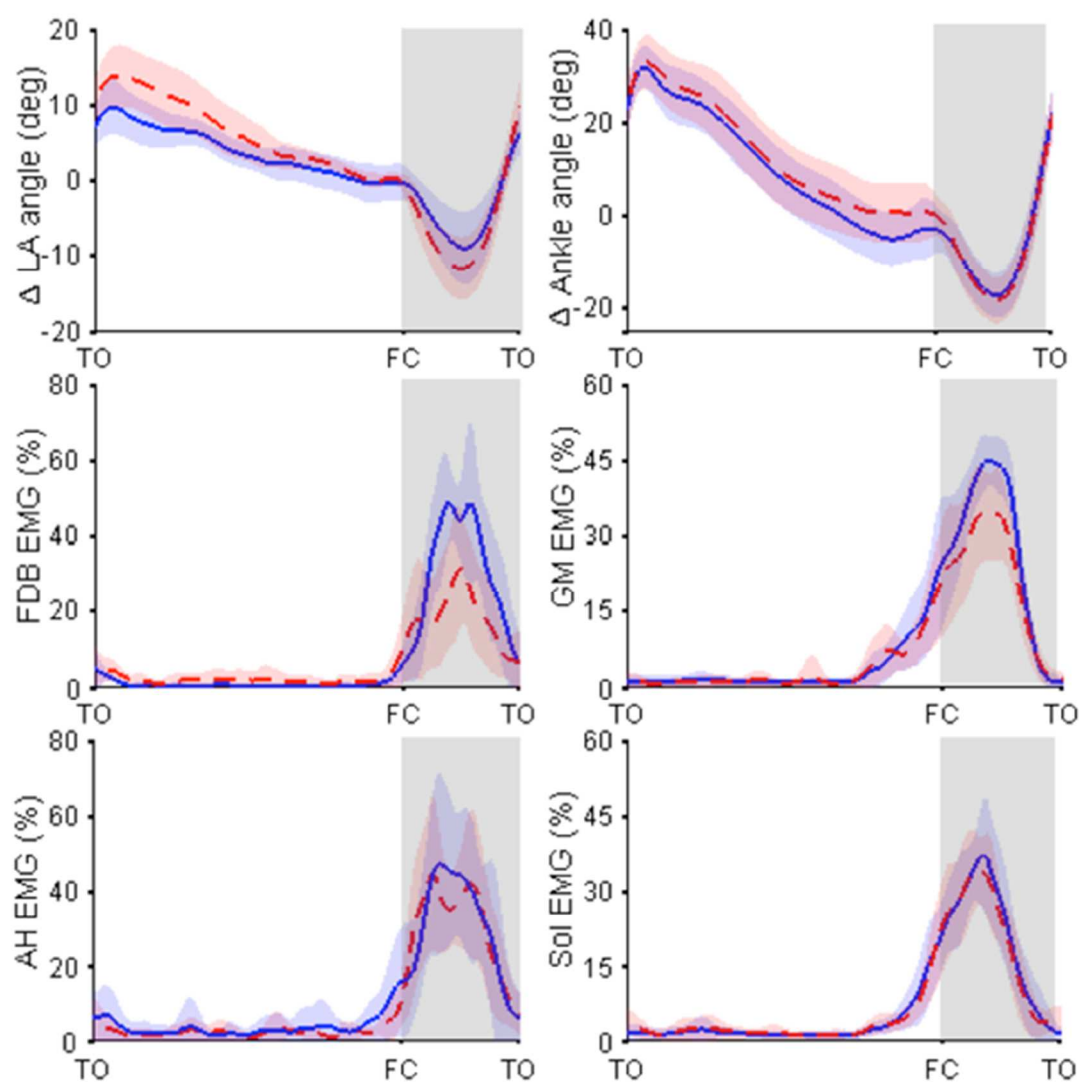


Figure 2. Group mean ensembles \pm standard deviation for changes (Δ) in longitudinal arch (LA) and ankle angle (degrees, $^{\circ}$, top), electromyography (EMG) root mean square signal amplitude for flexor digitorum brevis (FDB) and abductor hallucis (AH), gastrocnemius medialis (GM) and soleus (Sol). Group mean ensembles are defined from toe off (TO) to ipsilateral toe off for the right foot. Data recorded during running at 3.89 ms^{-1} . For each muscle EMG data is normalised to the maximal amplitude recorded for all trials. Change LA and ankle angle is calculated by offsetting the angle at heel contact in the barefoot condition, respectively. FC, foot contact

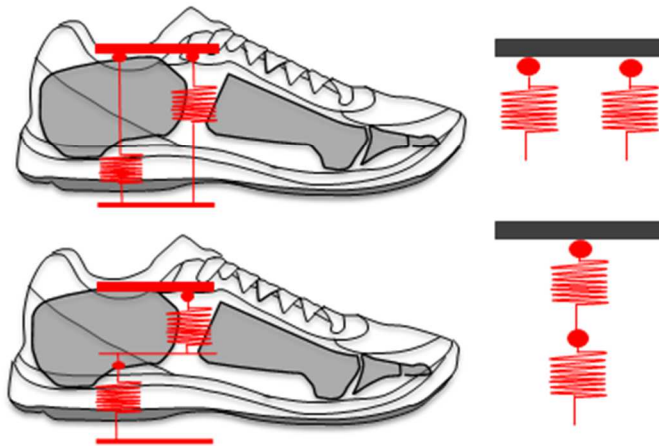


Figure 3. Depiction of a parallel (top) and in-series (bottom) spring arrangement between the longitudinal arch and running shoe. Both the longitudinal arch and running shoe will behave in a spring-like manner during running, compressing and recoil as force is applied and removed. If the longitudinal arch and running shoe act in-parallel, wearing a running shoe will increase the overall stiffness of the foot. If the longitudinal arch and running shoe act in-series, wearing a running shoe will increase the overall compliance of the foot. Based on the assumption that constant foot stiffness is favoured during steady state running, the response of the intrinsic foot muscles in regulating the stiffness of the arch will vary depending on whether the longitudinal arch and running shoe behave in-parallel or in-series.

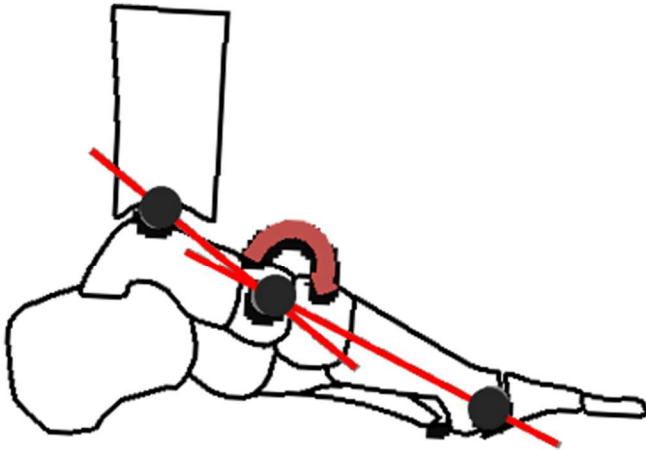


Figure 4. Longitudinal arch angle is defined as the angle created by the bisection of a vector projecting from a marker located on the medial malleolus to a marker located on the navicular tuberosity, with a vector projecting from a marker located on the head of the first metatarsal to a marker on the navicular tuberosity. A reduction in longitudinal arch angle indicates arch compression, while an increase in arch angle indicates arch recoil.