

1 **Flow Regime Identification for Air Valves Failure** 2 **Evaluation in Water Pipelines Using Pressure Data**

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11 **Abstract:** Air valve failure can cause air accumulation and result in a loss of carrying capacity, pipe
12 vibration and even in some situations a catastrophic failure of water transmission pipelines. Air is most
13 likely to accumulate in downward sloping pipes, leading to flow regime transition in these pipes. The
14 flow regime identification can be used for fault diagnosis of air valves, but has received little attention
15 in previous research. This paper develops a flow regime identification method that is based on support
16 vector machines (SVMs) to evaluate the operational state of air valves in freshwater/potable pipelines
17 using pressure signals. The laboratory experiments are set up to collect pressure data with respect to the
18 four common flow regimes: bubbly flow, plug flow, blow-back flow and stratified flow. Two SVMs are
19 constructed to identify bubbly and plug flows and validated based on the collected pressure data. The
20 results demonstrate that pressure signals can be used for identifying flow regimes that represent the
21 operational state (functioning or malfunctioning) of air valves. Among several signal features, Power
22 Spectral Density and Short-Zero Crossing Rate are found to be the best indicators to classify flow regimes

23 by SVMs. The sampling rate and time of pressure signals have significant influence on the performance
24 of SVM classification. With optimal SVM features and pressure sampling parameters the identification
25 accuracies exceeded 93% in the test cases. The findings of this study show that the SVM flow regime
26 identification is a promising methodology for fault diagnosis of air valve failure in water pipelines.

27 **Keywords:** Water transmission Pipeline; Air valve; Flow regime identification; Support vector machine;
28 Fault diagnosis

29 **1 Introduction**

30 Freshwater resources are unevenly distributed temporally and spatially and particularly
31 mismatching with urbanization development, thus leading to severe imbalance between supply and
32 demand. Many long-distance water transmission pipelines were built to address this type of problem,
33 such as in the case of the Snowy Mountains Hydro-electric Scheme in Australia (Bergmann, 1999), the
34 Great Lakes Basin Water Diversion (Becker and Easter, 1995), the Central Valley Project in the USA
35 (Mariño and Loaiciga, 1985), and South to North Water Diversion Project in China (Barnett et al., 2015;
36 Yu et al., 2018). In the pressurized water transmission pipeline, air valves are a common component
37 which is used to deaerate the pipe (Meng et al, 2016; Pothof and Clemens, 2012). The existence of air in
38 water pipelines will not only decrease water conveyance capacity and increase head losses (Escarameia,
39 2007; Lubbers, 2007), but could also lead to pipe vibration due to the pressure fluctuation of air-water
40 mixing flows. Worse still, it may even cause pipe to burst during the hydraulic transient process (Pothof
41 and Clemens, 2010). Air is most likely to accumulate in the downward sloping water pipe, which can
42 usually be removed by flowing water or discharged through air valves (Escarameia, 2007). If the water
43 velocity is lower than the “clearing velocity” (Kalinske and Bliss, 1943; Kent, 1952; Wisner et al, 1975),

44 the air cannot be completely taken away by hydraulic actions, therefore, air valves are essential for
45 removing air in this situation. Air valves often break down due to blockage in the vent hole or valve-
46 stem rupture caused by pipe vibration (Ramezani et al, 2015). However, air valves that are normally
47 located at the high spots of water conveyance pipelines are inconvenient to inspect and maintain (Pothof
48 and Clemens, 2012). Moreover, air valve failures cannot be easily detected and rectified, affecting the
49 performance of the pipeline.

50 Fault diagnosis of air valves located in mechanical systems (e.g., diesel, compressor) is often
51 performed by various pattern recognition algorithms based on the analysis of acoustic and/or vibration
52 signals (Pichler et al, 2011; Qin et al, 2012; Verma et al, 2011). However, acoustic and vibration signals
53 are not suitable for fault diagnosis of air valves in water conveyance pipeline due to poor working
54 conditions (e.g. humid underground, limited power and communication, and external disturbance)
55 (Stephens et al., 2004; Schwaller and van Zyl, 2015). However, pressure signals have been successfully
56 employed in valve fault diagnosis in mechanical systems (Feng et al, 2011). In the downward sloping
57 water pipes, when the air valves are out of service, the air accumulation can lead to flow regime transition.
58 This in turn can lead to the change in the dynamic behavior of the valve and pressure fluctuations in the
59 air-water flow. Moreover, pressure signals in the water pipeline are commonly available, therefore, this
60 study investigates their use to identify flow regime changes and detect the operational state of air valves
61 in downward sloping water pipes.

62 Flow regime identification has been widely studied in the literature. Numerous investigators have
63 applied various types of instruments to collect different data (e.g., flow image, void fraction or

64 differential pressure) for flow regime identification (Arvoh et al, 2012; Lee et al, 2008a,b; Roshani et al,
65 2015; Salgado et al, 2010). The features, e.g., frequency, stochasticity, fractals or chaotic time series
66 characteristics, are extracted from the data in order to improve the identification accuracy for a specific
67 application (Cai et al, 1994; Elperin and Klochko, 2002; Franca et al, 1991; Sun et al, 2013; Vince and
68 Lahey, 1982).

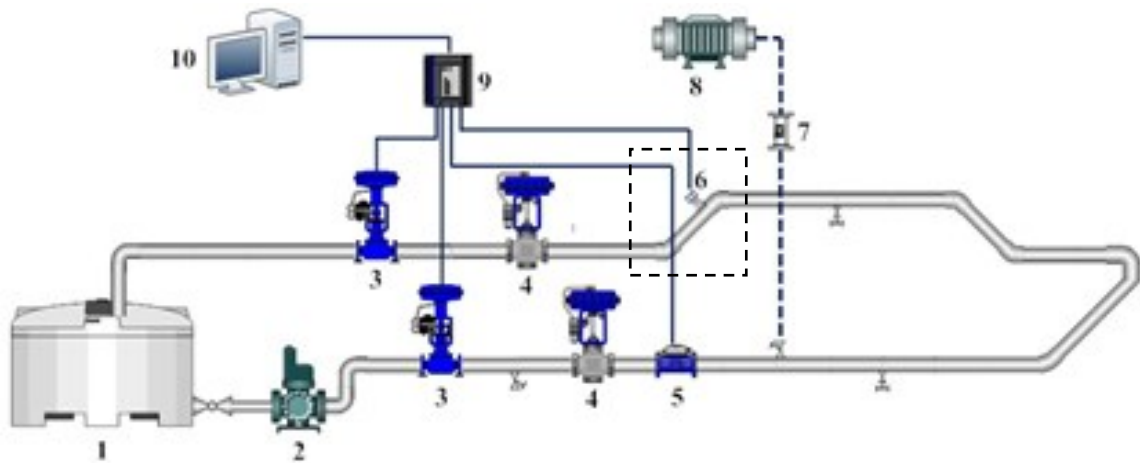
69 Moreover, identification of signal features (pattern recognition) can utilize the classification
70 methods, i.e., distinguishing the features of anomaly events from a spectrum of event sets. (Mi et al,
71 2001; Roshani et al, 2015; Tan et al, 2007). Support vector machines (SVM) and artificial neural
72 networks (ANN) are probably the most commonly used pattern recognition methods. SVM are less prone
73 to being trapped in a local minimum and require less data during the training process, but most
74 importantly can overcome the key weakness of ANN, which require an appropriate structure to be
75 selected and optimized for the problem at hand (Yang et al., 2017). In the water sector, SVM has been
76 used for water quality classification as an early warning tool. For example, a least square support vector
77 machine (LS-SVM) was combined with fuzzy clustering to estimate water quality failures in water
78 distribution networks (Aydogdu and Firat, 2015; Modaresi and Araghinejad, 2014). Moreover, SVM is
79 used for anomaly detection in water distribution systems based on the pressure and flow signals (Mounce
80 et al, 2011). In addition to classification applications, SVM is also applied in precipitation and runoff
81 predictions (Ahmadi et al, 2015; Bray and Han, 2004). These applications prove that SVM has a strong
82 capability as a classification tool. In this study, SVM is used for flow regime identification in water pipes,
83 whereby the flow regime changes could be used for diagnosing air valve operation states.

84 This paper aims to evaluate the operational state of air valve in the downward sloping water pipe
85 based on pressure data using SVM classification. Laboratory experiments are set up to collect the
86 pressure data. Then the data are used to train and validate SVM models. Bubbly flow (including quasi-
87 pure water state) or plug flow can be classified amongst all flow regimes through the SVMs. According
88 to the analysis of experimental data and the SVM-based results, the following aspects are addressed by:
89 (i) analysis of the optimal time-frequency characteristics of pressure signals corresponding to different
90 flow regimes in downward sloping water pipes, (ii) identification accuracy of SVM models using the
91 different features extracted from pressure data, and (iii) parameter analysis of SVM input data (e.g.
92 optimal sampling rate and time)? This paper presents a novel methodology for flow regime identification
93 in water pipe systems. Flow regime in a water pipe can then directly be linked to the operational state of
94 the air valve, thus performing air valve fault diagnosis and ensuring the safety of water pipelines. The
95 findings of this study can also provide potential guidance for parameter estimation of the SVM
96 classification model.

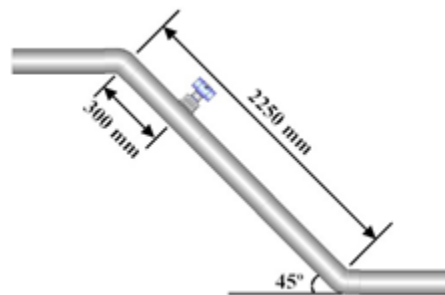
97 **2 Experimental facility**

98 A single-pipe transmission system is set up to collect the pressure signal data under the various flow
99 conditions. As shown in Fig. 1, the experimental set-up is based on a circulating water system pressurized
100 by a pump. All pipes are made of plexiglas, and the total length of the pipeline is about 80 m. The inner
101 and outer diameters of the pipes are 90 mm and 110 mm, respectively. To simulate air-water two-phase
102 flow in downward slope, the air was injected into the upstream of the pipeline by an air compressor. The

103 digital signals of pressure sensor and ultrasonic flowmeter are collected by a multiple-channel data
 104 acquisition card (Advantech USB-4711A).



105
 106 Fig. 1 Diagram of the test rig used in this study (test section is shown in the dashed box) - 1: water tank; 2: pump;
 107 3: electric valve; 4: pneumatic butterfly valve; 5: ultrasonic flowmeter; 6: pressure sensor; 7: gas rotameter; 8: air
 108 compressor; 9: data acquisition instrument; 10: computer



109
 110 Fig. 2 A detail of the test section with the pressure sensor

111 The tested pipe section in downward slope is illustrated in Fig. 2. The length of the test section is
 112 2,250 mm, and the pressure sensor is deployed at 300 mm away from the upstream elbow. The
 113 measurement range of the pressure sensor is 0~200 kPa with an accuracy of 0.2%. The experimental
 114 procedure includes the following aspects:

115 1) The planned water velocity range included 16 different values (0.7, 0.9, 1.1, 1.3, 1.5, 1.7, 1.8,
116 1.9, 2.0, 2.1, 2.2, 2.3, 2.4, 2.5, 2.6 and 2.7 m/s), which were controlled by the electric valve near the
117 pump. The exact value of the velocity was then measured by the ultrasonic flowmeter.

118 2) The air flow measured by the gas rotameter was set to 8 discrete values (0.5, 1.0, 1.5, 2.0, 2.5,
119 3.0, 3.5 and 4.0 m³/h), which was controlled by the outlet valve at the air compressor.

120 3) A total of 128 cases were tested during the experiment based on the orthogonal combination of
121 different water velocities and air flow values.

122 4) The pressure signals were sampled at a frequency of 1 kHz and the sampling time was set to 20
123 s.

124 5) The images of air-water flow regime at the test section were recorded by a high-speed camera
125 from a side view.

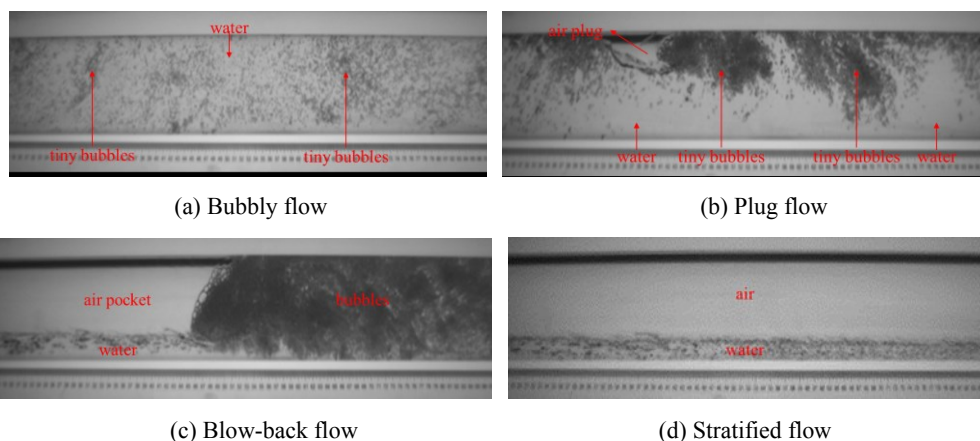
126 **3 Methodology**

127 3.1 Description of Flow Regimes

128 It is known that four flow regimes may appear in the downward sloping water pipes (Pothof and Clemens,
129 2011). Those can be seen in the images of obtained in the tests, as shown in Fig. 3. It should be noted
130 that the camera lens is placed in parallel with the longitudinal pipe axis, thus the pipes in the images
131 appear to be horizontal.

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Fig. 3 Typical flow regime images

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There is always a small amount of dissolved air in the water, which can be assumed as a state of

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“quasi-pure water” (Zhu et al, 2018). Although the amount of dissolved air is very small, the effect of

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local resistance by the elbow will aggregate it into tiny bubbles that are dispersed in pipes (Barnea, 1986).

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Therefore, bubbly flow (Fig. 3a) can be considered the normal flow regime in the downward sloping

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water pipes. When the water velocity is lower than “clearing velocity”, small bubbles will accumulate to

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create plug flow (Fig. 3b), and the air plugs will finally be discharged out of the pipe if the air valve is

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working normally. However, if the air valve is not working properly, the air plugs will gradually coalesce

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into a large air pocket at the top of the slope, which is called “blow-back flow” as shown in Fig. 3c. As

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the large air pocket continues to expand until occupying the entire slope, stratified flow occurs with the

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water flowing beneath the air (Fig. 3d). According to the flow regime analysis, the occurrence of blow-

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back flow or stratified flow in downward sloping pipes indicates that the air valve may be malfunctioning.

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3.2 SVM-based Flow Regime Identification

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Classification is a process of classifying data points into specific groups (or classes). SVM is one of the

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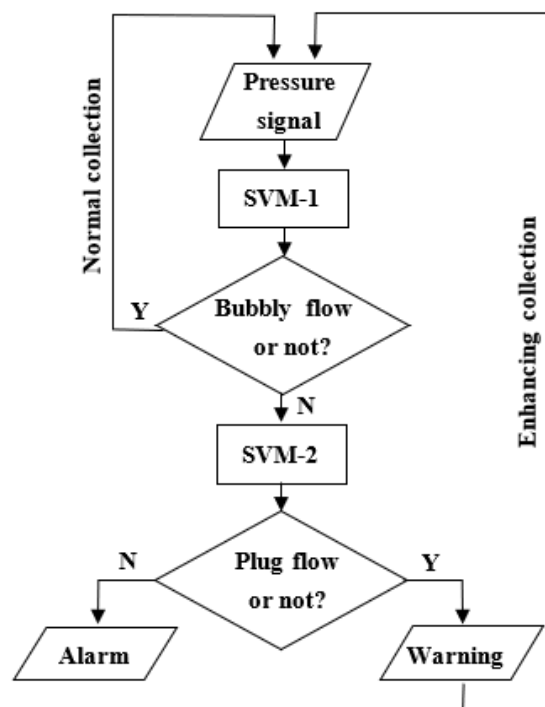
powerful methods for data classification. The training process of a SVM classifier involves finding the

152 best hyperplane that divides the two classes with the given data points. If it is necessary to divide the
153 data points into n classes, $n-1$ hyperplanes should be constructed by the classifier. The original maximum-
154 margin hyperplane algorithm proposed by Vapnik (1963) is used to build a linear classifier and can only
155 solve linearly classification problems. In this paper, we used the maximum-margin method, proposed by
156 Boser et al. (1992), to deal with the nonlinear classification problems by a spectrum of linear decision
157 functions separating hyperplanes in a transformed high-dimensional feature space. The transformation
158 algorithm is similar to the mapping calculation except dot product which is replaced by a nonlinear kernel
159 function (Boser et al., 1992). For a specific nonlinear classification problem, an appropriate kernel
160 function is crucial for the classification performance, and therefore the Radial Basis Function (RBF)
161 (Ring and Eskofier, 2016) is used as kernel functions through several trials.

162 The flow regimes of blow-back or stratified flows are the most severe situations of air accumulation
163 in pipelines, which indicates air-valve is likely to fail completely. Although plug flow regime shows the
164 less volume of air accumulation than blow-back and stratified flows, the frequent occurrence of plug
165 flow indicates potential drawbacks for air exhausting (e.g., the insufficient number of air valves).
166 Therefore, the four flow regimes are hierarchically classified into three categories for improving the
167 identification accuracy, since both the blow-back and stratified flows are considered in the same
168 category. Fig. 4 shows the flowchart of the flow regime identification. As can be seen in Fig. 4, two SVM
169 models have been constructed to identify the different flow regimes: 1) SVM-1, which is used to
170 distinguish bubbly flow (including quasi-pure water state) from the other three flow regimes; and 2)

171 SVM-2, which is used to distinguish plug flow from blow-back and stratified flows. The detailed training
 172 and testing process are introduced in the following section.

173 According to Fig. 4, pressure signals are collected with low frequency (twice a day, for example)
 174 at normal conditions. The sampling frequency (i.e. sampling times per minute) will be conducted and
 175 maintained continuously when the results of SVM-1 classification demonstrates bubbly flow. If the
 176 results of SVM-1 are not identified as the quasi-pure water state or bubbly flow, the features abstracted
 177 from pressure signals will be passed as input to SVM-2. When the SVM-2 classification results in the
 178 plug flow classification, a “Warning” signal will be given and then the sampling frequency of pressure
 179 signals should be increased in order to strength the monitoring of the transition process from plug flow
 180 to blow-back and stratified flows. Once the results of SVM-2 classification does not show plug flow, an
 181 “Alarm” signal will be launched, which indicates the potential failure of air valve.



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Fig. 4 Flowchart of the evaluation of air valve exhaust

184 3.3 SVM Training and Testing

185 Among the entire 128 cases, two cases were not used for SVM analysis due to the faulty data acquisition
 186 card (one for blow-back flow and the other for stratified flow). Among the remaining 126 cases, there
 187 are 69, 34, 18 and 5 cases for bubbly flow, plug flow, blow-back flow and stratified flow, respectively.
 188 These were determined by analyzing flow regime photos (see Fig. 3). SVM-1 is trained based on 94
 189 cases, and the remaining 32 cases are used to test the identification accuracy of SVM-1. SVM-2 is trained
 190 based on 42 cases exhibiting the three characteristic flow regimes (plug flow, blow-back flow and
 191 stratified flow). The remaining 15 are used to test the identification accuracy of SVM-2. The SVM
 192 training and testing in this study are performed on the Matlab R2011b platform, and the procedures of
 193 SVMs training and testing can be described as follows:

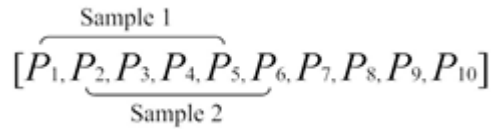
194 1) Pressure data are preprocessed by downsampling, which can change the sampling rate of the
 195 original pressure signal.

196 2) In order to make the model training and the obtained testing accuracy more reliable, it is
 197 necessary to enlarge the data volume for both SVM training and testing. This is done by dividing data
 198 series based on the same interval. Assuming that the total length of one pressure signal series is L , the
 199 length of one sample is L' , and the interval between the adjacent samples is I , the number of samples
 200 (N) in a pressure signal series can be calculated by:

$$201 \quad N = \left\lceil \frac{(L - L')}{I} \right\rceil + 1 \quad (1)$$

202 Fig. 5 shows the example of how samples are created from one pressure data series in this study. As can
 203 be seen in Fig. 5, the total data volume of one pressure signal [P_i] is 10. The length of one sample is 5.

204 The interval between two adjacent samples is 1. In Fig. 5, the first sample is from P_1 to P_5 , and the last
 205 sample is from P_6 to P_{10} . Hence the total number of samples is 6, which is equal to the result calculated
 206 by Eq. (1).



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Fig. 5 Samples for an experimental process

209 3) Every training and testing sample is labeled with 1 or 0, which indicates whether it belongs to a
 210 given category.

211 4) The SVMs are trained based on the features extracted from the training samples. The pressure
 212 signals with respect to different flow regimes have significant differences in terms of three types of
 213 features, i.e., pressure fluctuation, periodicity and frequency distribution. The features and their types are
 214 listed in Table 1.

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Table 1. Features for flow regime identification

Feature type	Feature name	Abbreviation
Pressure Fluctuation	Variance	V
	Short-time Zero-crossing Rate	SZR
Periodicity	Autocorrelation Coefficient	AC
	Hilbert-Huang Transform	HHT
Frequency Distribution	Power Spectrum Density	PSD

216 In Table 1, Variance (V) can reflect the amplitudes of pressure signals for different flow regimes.

217 Short-time Zero-crossing Rate (SZR) is the rate at which the pressure signal changes from positive to

218 negative within a short period of time after subtracting their mean values. Autocorrelation Coefficient

219 (AC) is a feature vector which consists of 51 autocorrelation coefficients, since each test lasts 2 seconds

220 including 51 samples. Hilbert-Huang Transform (HHT) is an algorithm that decomposes a signal into
221 various components for obtaining the instantaneous frequency (Ding et al, 2007). The frequency band in
222 the range of 0 to 10 Hz is evenly divided into 5 components. Each frequency band is 2 Hz here. The
223 remaining frequency range (> 10 Hz) belongs to the 6th component. Six eigenvalues (i.e., components)
224 therefore exist in the feature vector of HHT. With respect to Power Spectrum Density (PSD), the pressure
225 signal value is normalized by subtracting the mean value to eliminate the interference of the average
226 pressure. Then the Nyquist rate (using half of the sampling rate, 500 Hz) is equally divided into 128
227 frequency bands, where the average size of frequency band (i.e. frequency interval) is about 3.9 Hz. The
228 129 eigenvalues are included in the feature vector of PSD. Both HHT and PSD are the frequency-domain
229 features. Since the feature extraction of HHT is more time-consuming than PSD, the number of frequency
230 bands in the HHT feature is less than that of PSD. The frequency bands of HHT and PSD are set
231 differently which will be discussed in 4.1.2.

232 5) The accuracy of the SVM classification for flow regime identification is investigated using the
233 experimental samples. The RBF is used as the kernel function in the SVM model and the parameters of
234 SVM are estimated by the Sequential Minimal Optimization (SMO) method during each training (Platt,
235 1998).

236 **4. Results and Discussion**

237 4.1 Time-frequency Analysis of Experimental Data

238 Flow regimes in water pipes are different from those in other media (e.g., oil-gas transportation, chemical
239 pipelines or nuclear reactors) (Crawford et al, 1985). Therefore, the time-frequency characteristics of
240 pressure signals of different flow regimes need to be analyzed for flow regime identification.

241 *4.1.1 Time-domain Characteristics of Pressure Signal*

242 Four typical cases are selected to show the time-series pressure signals of different flow regimes in Fig.
243 6. q_a refers to the air flow and v_w represents the water velocity. As shown in Fig. 6a, the pressure
244 fluctuation of bubbly flow is relatively stable. Because there is little amount of air in bubbly flow, the
245 interaction between air and water phases is not strong. In the plug flow case (Fig. 6b), the air plug moves
246 up and down due to its volume change or deformation, and thus the pressure signal of the plug flow
247 shows occasional pressure drops. In Fig. 6c, the characteristic of pressure fluctuation of blow-back flow
248 is similar to that of plug flow, but the changes in the pressure drop are more pronounced. The greater
249 volume of air has been distributed throughout the downward slope with respect to stratified flow, and the
250 air-water interface intermittently flows back into the slope. Hence, the pressure of stratified flow
251 fluctuates periodically, as shown in Fig. 6d. Fig. 6 also demonstrates that the amplitudes of pressure
252 fluctuation of the stratified flow is the largest one, while the second largest is the blow-back flow. In
253 order to further confirm this result, the variance analysis of all the pressure signals is conducted to express
254 the amplitude of pressure changes.

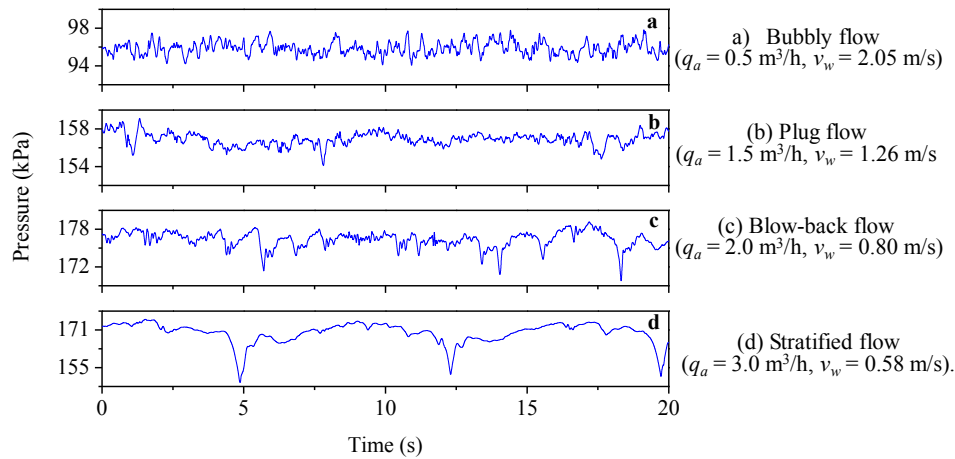
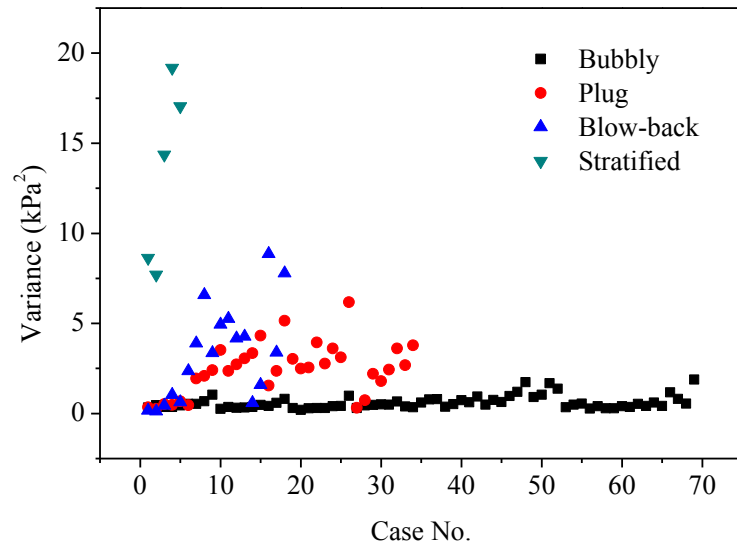


Fig.6 Time-domain pressure signals of different flow regimes

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258 Fig. 7 shows the variances of all pressure signals collected in the tests. As shown in Fig. 7, the
259 variances of all the pressure signals with respect to different flow regimes can be ranked in a descending
260 order as follows: stratified flow, blow-back flow, plug flow and bubbly flow. That is because the
261 transition in flow regime is closely related to the change of the air fraction, and it is generally accepted
262 that bubbly flow, plug flow, blow-back flow and stratified flow appear sequentially in the downward
263 sloping water pipe as the air fraction increases (Pothof and Clemens, 2011). Moreover, the pressure
264 fluctuation of air-water flow will become increasingly intense with the increase of air content when the
265 air fraction is lower than 50% (Riverin et al, 2006). According to the test conditions, the maximum air
266 fraction in our tests was 25%. Thus, the amplitude of pressure fluctuation in stratified flow is the largest
267 among the four regimes, which is followed by blow-back flow, plug flow and bubbly flow in order. As
268 a result, the variance of pressure signal (in Table 1) can be used as an index (feature which can be input
269 into the SVM) for flow regime identification.



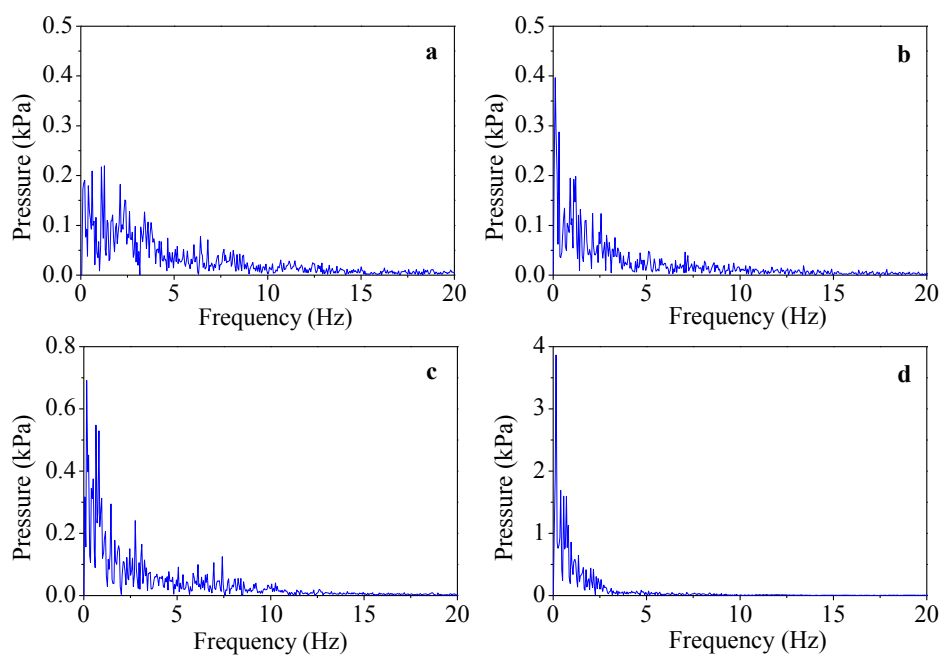
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Fig. 7 Variances of all the pressure signals

272 4.1.2 Frequency-domain Characteristics of Pressure Signal

273 Fig. 8 shows the results of Fast Fourier Transform (FFT) on the pressure fluctuation signals according to
 274 the four typical cases in Fig. 6. The pressure fluctuation signals can be obtained by subtracting the mean
 275 values from the original pressure signal values.



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Fig. 8 Fourier spectra of pressure signals for different flow regimes (a) bubbly flow, (b) plug flow,
 (c) blow-back flow, (d) stratified flow.

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279 As shown in Fig. 8, the frequency-domain distributions of four typical cases are mainly shown
280 within 10 Hz, therefore the frequency-domain analysis on pressure signals should focus on this frequency
281 range when the frequency-domain feature is used for flow regime identification. The frequency features
282 of HHT and PSD used in this study are set with the frequency bands of 2 Hz and 3.9 Hz, respectively.
283 Moreover, the frequency-domain distributions of pressure fluctuation signals show the single-peak
284 characteristic in Fig. 8 except for bubbly flow (Fig. 8a), which indicates the pressure fluctuations of plug
285 flow, blow-back flow and stratified flow have more significant periodicity in time-domain. It can also be
286 seen in Fig. 8 that the single-peak characteristic becomes increasingly obvious and the pressure value of
287 the peak increases when comparing from Fig. 8b to Fig. 8d. The main frequency components (i.e.
288 pressure peak) are 0.2 KPa, 0.4 KPa, 0.7 KPa, 3.7 KPa in Figs 8a-8d, respectively. It indicates the
289 periodical characteristic of the pressure signals based on the main frequency components becomes more
290 significant as the air fraction increases. Consequently, the feature AC representing periodicity is used for
291 flow regime identification (shown in Table 1).

292 4.2 SVM-based Flow Regime Identification

293 4.2.1 Effect of Pressure Signal Features on Identification Accuracy

294 The identification accuracy is defined as the ratio of the number of samples that are correctly classified
295 into the specific flow regime by the SVM model to the total number of samples. Before studying the
296 effect of pressure signal features on identification accuracy, the original pressure signals are first

297 downsampled to 200 Hz, therefore, the length of one set of pressure signal (L) is 4000. The sample length
 298 (L) is set to 1000, which means the sampling time (the ratio of sample length to sampling rate) is 5 s.
 299 The interval between the adjacent samples (I) is 200, so every set of pressure signal can obtain 16 samples
 300 for SVM training or testing. The training data mentioned in Section 3.3 are used to train the SVM models,
 301 while the testing data are used to investigate the identification accuracy in SVM models. The
 302 identification accuracies of different features and their combinations for SVM-1 and SVM-2 are listed in
 303 Table 2.

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Table 2. Flow identification accuracies corresponding to different features

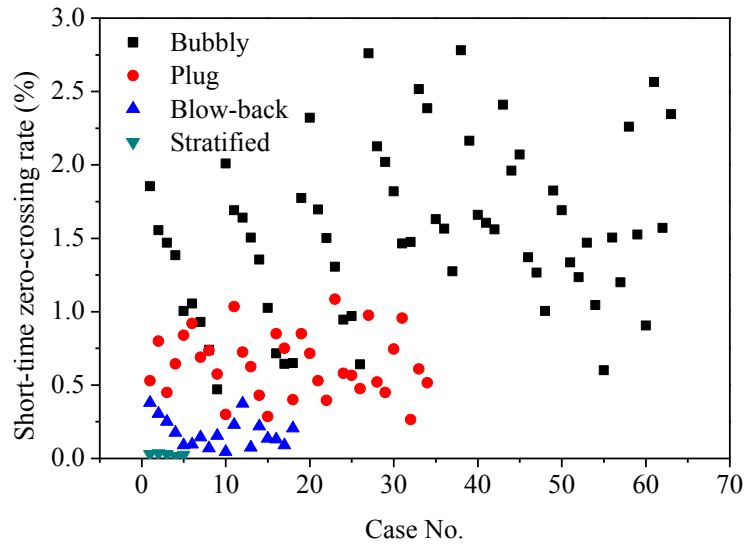
Feature	SVM-1	SVM-2	Feature	SVM-1	SVM-2
SZR	89.6%	80.4%	SZR+V	89.8%	80.9%
V	82.5%	70.7%	AC+ PSD	79.0%	77.3%
AC	87.1%	73.3%	V+PSD	89.2%	87.1%
HHT	73.5%	83.1%	V+AC	88.1%	74.2%
PSD	89.2%	87.6%	SZR+AC+PSD	79.0%	76.0%
SZR+PSD	88.5%	85.8%	SZR+V+PSD	88.5%	85.8%
HHT+PSD	81.7%	73.8%	V+AC+PSD	78.8%	76.9%
SZR+AC	89.2%	83.1%	SZR+V+AC+PSD	78.8%	75.6%

305 As shown in Table 2, the comparative results show that SZR combined with V provide only a
 306 marginal improvement over using only SZR for SVM-1 classification, while the PSD is the optimal
 307 feature for SVM-2. Therefore, SZR and PSD are the best individual features for SVM-1 and SVM-2,
 308 respectively. The features related to HHT perform worse than other parameters in accuracy comparisons
 309 for both SVM-1 and SVM-2, and HHT calculation is computationally demanding. Thus HHT is not
 310 recommended to use for flow regime identification. As can be seen from Table 2, when comparing the
 311 identification accuracy of AC and AC-related feature combinations, SVM-1 is superior to SVM-2.

312 In order to explain the reason why SZR and PSD have better performance on identifying flow
313 regimes as input features, the SZR values derived from all the original pressure signals in all cases are
314 shown in Fig. 9 and the PSD distributions of four typical cases in Fig. 6 are demonstrated in Fig. 10. In
315 general, the SZR values can be ranked in term of the four flow regimes in descending order in Fig. 9:
316 bubbly flow, plug flow, blow-back flow and stratified flow. The SZR values in a few cases of bubbly
317 flow are mixed with those of plug flow, and thus the identification accuracy in SVM-1 that is only used
318 to classify bubbly flow cannot reach the higher values (the highest accuracy is 89.6%). SVM-2 is used
319 to classify plug flow which can mix both bubbly flow and blow-back flow in Fig. 9, and thus the
320 identification value of SZR decreases further (equal to 80.4%) when only SZR is used as input feature in
321 SVM-2. Additionally, it is distinct between stratified and blow-back flows associated with SZR values,
322 and however they cannot be an indication of flow regime transition in SVM due to the limited
323 experimental samples.

324 Fig. 10 shows the PSD results of the pressure signals according to the four typical cases from Fig.
325 6. The PSD feature is a vector that consists of 129 eigenvalues based on the fixed frequency bands. The
326 PSD distribution of stratified flow in the high frequency range (>50 Hz) shows periodical changes and
327 distinguishes from other three flow regimes. The key difference between plug and blow-back flows in
328 PSD distribution lies in the low frequency range (< 50 Hz). The bubble flow shows relative values of
329 PSD when the frequency bands are larger than 100 Hz. Therefore, it indicates the PSD as input feature
330 in SVM models would perform well. Although only four cases of different flow regimes are chosen here
331 to show the difference in PSD distributions, other cases of PSD have also been investigated in this study.

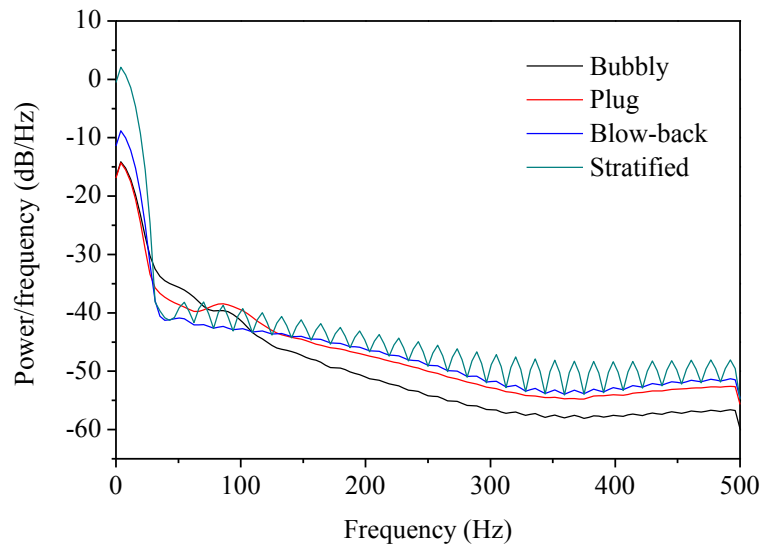
332 The results show the similar rules associated with PSD. Based on the above analysis, SZR and PSD are
 333 effective as input features for flow regime identification in SVM models, and the two features will be
 334 used for the sampling parameters study in the following section.



335

336

Fig. 9 Short-time zero-crossing rates (SZR) for all cases



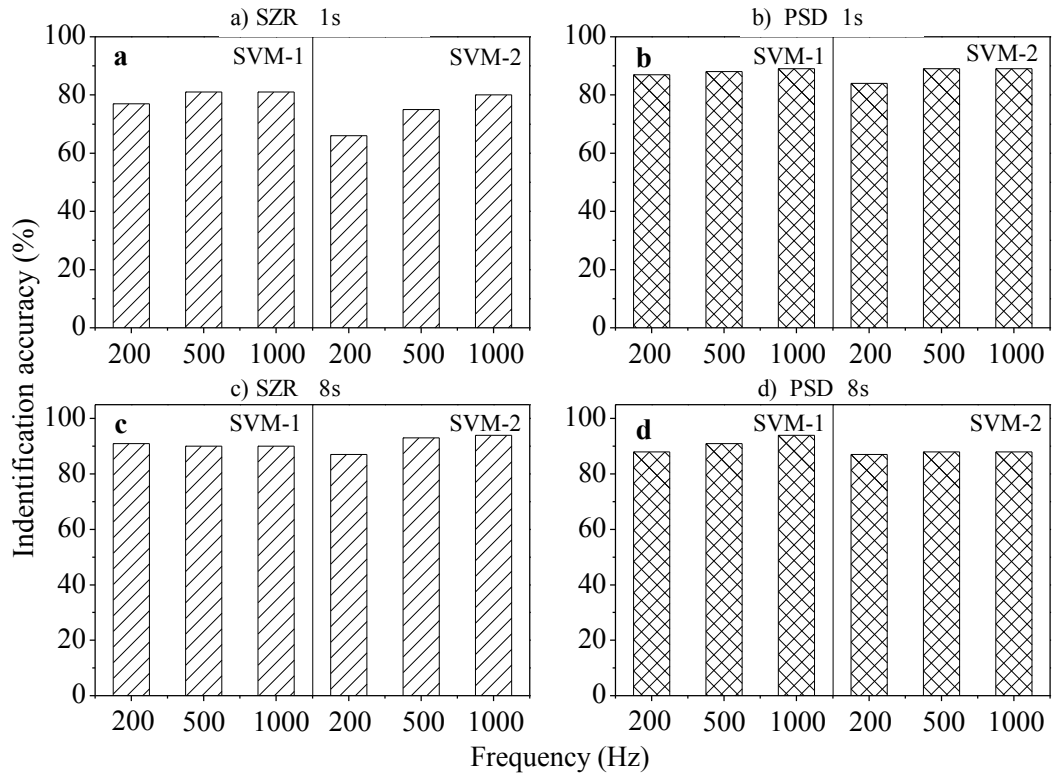
337

338

Fig. 10 PSD results of pressure signals for four typical cases

339 *4.2.2 Impact of Sampling Parameters on Identification Accuracy*

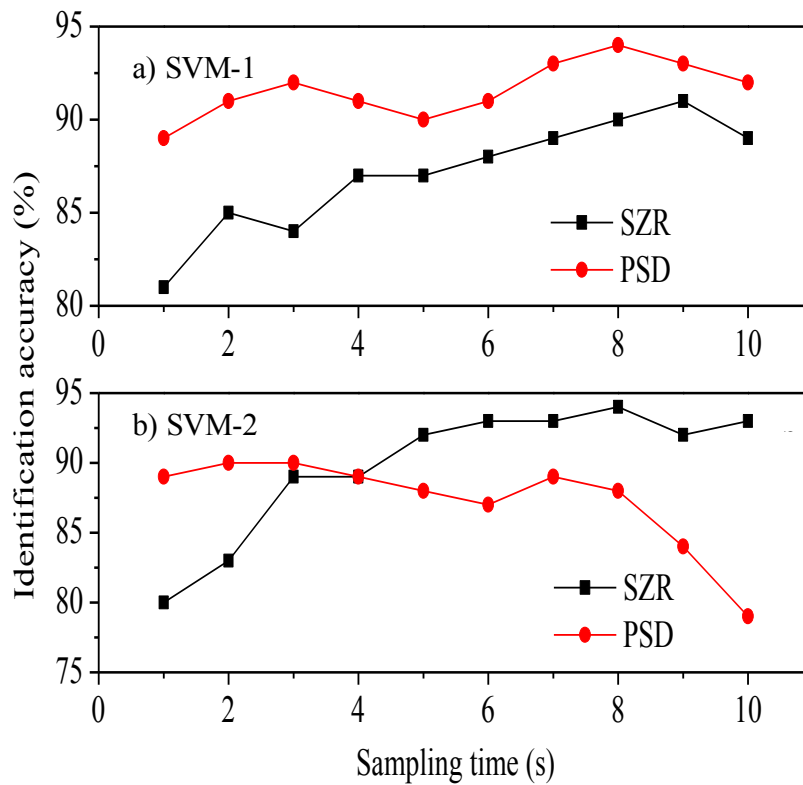
340 The sampling rate and sampling time can be adjusted by downsampling and changing the sample length
341 (L), respectively. With the features of SZR and PSD, the impact of sampling rate on identification
342 accuracy in SVM models is investigated when sampling time (1 s or 8 s, for example) is given. In order
343 to make a relatively large difference among all the samples, the overlapping proportion between the
344 adjacent samples should be as small as possible, therefore the interval between the adjacent samples in
345 this study is set to 1,000. Fig. 11 shows the effect of sampling rate on the flow regime identification
346 accuracy. The identification accuracy is generally improved (i.e. accuracy value increases consecutively)
347 with the increase in sampling rate. In some cases, sampling rate does not show significant impact on the
348 identification accuracy (SVM-1 in Fig. 11c). In Fig. 11c, the identification accuracy increases from 87%
349 to 94% for SVM-2 with the increase in sampling rate. In Fig. 11a, the identification accuracy has been
350 improved from 66% to 80% when SZR is used as the feature. It demonstrates that the identification
351 accuracy of SZR is more sensitive to the sampling rate than that of PSD, because higher sampling rates
352 can amplify distinctions of the SZR values among different flow regimes. Therefore, the sampling rate
353 of 1 kHz (the maximum value) is recommended for the applications of flow regime identification.



354

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Fig. 11 Impact of sampling rate on identification accuracy



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Fig. 12 Impact of sampling time on identification accuracy

358 In order to study the impact of sampling time on identification accuracy, the sampling rate is first
359 fixed to 1 kHz, and the results with different features (SZR and PSD) are shown in Fig. 12. In Fig. 12a,
360 the identification accuracies for both SZR and PSD show the rising trends with the increase of the
361 sampling time in SVM-1, however the identification accuracy of PSD is better than that of SZR.
362 Moreover, as mentioned before, the SZR values of some cases in bubbly flow are mixed with those in
363 plug flow. Hence the feature SZR is not the best feature for SVM-1 since SVM-1 is built to classify
364 bubbly flow from all flow regimes. As shown in Fig. 12b, the identification accuracy of SZR in SVM-2
365 ascends as the sampling time increases, however the PSD shows the opposite trend. As can be seen in
366 Table 1, SZR is a time-domain feature that can reflect the pressure fluctuation of air-water flow, and SZR
367 can distinguish plug flow from blow-back flow and stratified flow according to Fig. 9; while PSD can
368 reflect the frequency-domain distribution of the pressure signal, which can clearly differentiate bubbly
369 flow from the other three flow regimes by referring to Fig. 8 and Fig. 10. Therefore, it is concluded that
370 PSD is the optimal feature for SVM-1, and SZR is the optimal feature for SVM-2 under various sampling
371 time conditions. With the optimal features and sampling parameters (sampling rate: 1 kHz; sampling
372 time: 8 s), the results of Fig. 12 show that the best identification accuracies for SVM-1 and SVM-2 are
373 94.3% and 93.9%, respectively.

374 4.3 Discussion

375 In water transmission pipelines, pressure signals can be obtained with a lower cost compared with void
376 fraction (Arvoh et al, 2012; Lee et al, 2008b; Roshani et al, 2015; Salgado et al, 2010). If differential
377 pressure signal is adopted as the indicator to evaluate the operation state of air valves in water pipes, it

378 will be difficult to match an appropriate interval between the pressure taps, and therefore differential
379 pressure signal cannot accurately predict flow regimes (Sun, 2005). Accordingly, pressure signal is the
380 best indicator used to identify the operational state of air valves in water pipes.

381 The energy consumption of pressure signal collection with high frequency (> 100 Hz) can be
382 ignored in the air-water two-phase flows monitoring (Elperin and Klochko, 2002; Sun, 2005). The
383 sampling rate of 1 kHz is suggested to be used in practical applications, since the collected pressure
384 signals will contain the essential information which could amplify the distinctions in SZR and PSD for
385 different flow regimes.

386 According to the previous study by Lee et al. (2008a), instantaneous flow regime identification was
387 applied to practical applications indicating that the sampling time of 1 s could identify the flow regimes
388 successfully in the downward sloping pipe using the cross-sectional void fraction indicator. However, in
389 this study the sampling time of 8 seconds is found to give the best identification accuracy using the
390 pressure signal indicator. The possible reason is that only longer sampling time can reflect the dynamic
391 characteristics of air-water pressure fluctuation in the flow regime transition.

392 Due to the limitation of the experimental facility, the training data cannot cover all kinds of pipe
393 conditions and operational cases. The results of flow regime identification can be extended by more
394 experimental data. Moreover, the void fraction signal can be used in the same methodology, if void
395 fraction is measured via air valves. In that case, the better results of flow regime identification may be
396 obtained by integrating pressure and void fraction measurements.

397 **5 Conclusions**

398 This paper proposed a novel SVM method to identify flow regimes using pressure signals. Flow regimes
399 are closely related to air fraction in water pipes, and thus indicate operation state (functioning or
400 malfunctioning) of air valves. An experiment facility involving a transmission pipeline is set up with the
401 testing section that includes the pressure gauge on a segment of downward sloping pipe. Several features
402 including Variance (V), Short-time Zero-crossing Rate (SZR), Autocorrelation Coefficient (AC), Hilbert-
403 Huang Transform (HHT), Power Spectrum Density (PSD), are used to extract the information that
404 represents fluctuations, periodicity and frequency distributions from the collected pressure signals. The
405 combination of the features as inputs variables to the SVM models is investigated. Two SVM models are
406 set up for classifying four flow regimes, and the parameters in the SVM classification are examined for
407 improving the identification accuracy. The key conclusions are drawn:

408 1) For the analysis of collected pressure signals, the amplitude of pressure fluctuations for different
409 flow regimes can be sorted into a descending ordered list as follows: stratified flow, blow-back flow,
410 plug flow and bubbly flow. The periodicity of pressure fluctuations becomes more obvious as the
411 air fraction increases, and the periodical characteristics of pressure signals are distinct among
412 different flow regimes. In the analysis of frequency-domain distributions of pressure signals, the
413 fluctuation frequency of four typical flow regimes occurs within 10 Hz. The four flow regimes show
414 a strong variation trend in terms of pressure fluctuation.

415 2) SVM-1 is used to classify bubbly flow and then SVM-2 distinguish plug flow from blow-back and
416 stratified flows. PSD and SZR are found to be the best features for the SVM classification through

417 the combination analysis. The SVMs perform well for flow regime identification using the suitable
418 features as input variables.

419 3) The sampling parameters have a significant impact on the performance of SVM for identifying flow
420 regimes. Based on the experimental data, the pressure sampling rate should be set relatively high
421 (maximum 1 kHz) and the long sampling time is recommended to improve the identification
422 accuracy of SVMs (e.g., 8 s in this study). With the best SVM features (i.e., PSD and SZR) and the
423 optimal sampling parameters, the identification accuracy of SVM-1 and SVM-2 can reach 94.3%
424 and 93.9%, respectively.

425 Data and method in this paper have been collected and tested based on an in-door experimental facility.
426 The practical application of this flow regime identification method should be updated with the pressure
427 data to train the SVM models. In the future, some field tests of the method should be done to validate the
428 method. The high frequency pressure sensors which are used in the experiments should be adequately
429 installed in the real pipelines to carry out this flow regime identification approach. Other sensors (e.g.
430 acoustic or vibration sensors) are promising and can be used to extend this study.

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